Interaction diagram for columns with multi-spiral reinforcement: modeling and experimental evidence

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2 Computational model

3 Results







Computational model

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④ Conclusions

5 Goals for 2022

Introduction

back then in 2008

Semestrální práce na téma:

Interakční diagram železobetonového prvku obdélníkového průřezu



now in 2022

TAČR-MOST 2020-2022: Reducing material demands and enhancing structural capacity of multi-spiral reinforced concrete columns-advanced simulation and experimental validation

- 1 Software for the design and advanced FE modeling of reinforced concrete columns with the multi-spiral reinforcement (MSR)
- 2 Develop formulae for the robust yet efficient design of columns with MSR incorporating the effect of multiple-confined zones. Develop the interaction diagram for the design of columns with MSR

 Confined concrete → enhanced strength and ductility



Havlásek et al. (2022): Efficient Approach to Measuring Strength and Deformation of Passively Confined Concrete. Li, Wu 2016: Stress-strain behavior of actively and passively confined concrete under cyclic axial load.

- Confined concrete → enhanced strength and ductility
- Spiral reinforcement:
 - circular CS, higher strength + ductility, material savings
 - uniaxial compression only
- Multispiral reinforcement:
 - arbitrary shape of CS + material savings (43%) + manufacture (33%)
 - \searrow M+N+V



Yin et al. (2011): Interlocking Spiral Confinement for Rectangular Columns.



Samuel Yin: *Helical Rebar Structure* US 2004/0231278 A1 (Nov. 25, 2004).

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- Confined concrete → enhanced strength and ductility
- Spiral reinforcement:
 - circular CS, higher strength + ductility, material savings
 - high uniaxial compression only
- Multispiral reinforcement:
 - arbitrary shape of CS + material savings (43%) + manufacture (33%)
 - \rightarrow M+N+V



P. Havlásek et al. (2021): Modeling of precast columns with innovative multispiral reinforcement. Data from M. Kuo (2008): Axial Compression Tests and Optimization Study of 5-Spiral Rectangular RC Columns.

- Confined concrete → enhanced strength and ductility
- Spiral reinforcement:
 - circular CS, higher strength + ductility, material savings
 - uniaxial compression only
- Multispiral reinforcement:
 - arbitrary shape of CS + material savings (43%) + manufacture (33%)
 - Second secon
- Design codes for conventional reinforcement
- No recommendations for MSR, absence of data

- → Conduct experiments: M+N, monotonous loading
- → Develop and validate computational model, compute interaction diagram
- → Use FEM results for formulation of formulae for engineers



Experiment



e = 0, 50, 100, 150, 200 mm

- $f_c = 43.0 \text{ MPa}$ $E_{S,40} = 26.9 \text{ GPa}$ $f_y = 420 \text{ MPa}$
- $\rho_V = 2.00\%$ $\rho_L = 2.51\%$ $\sigma'_L = 5.65 \text{ MF}$
- σ'_{μ} = 5.65 MPa σ'_{s} = 7.82 MPa



B = 400 mm, c = 20 mm, H = 60 mm $d_L = 360 \text{ mm}, D_L = 13 \text{ mm}, k_{e,L} = 0.91$ $d_S = 120 \text{ mm}, D_S = 10 \text{ mm}, k_{e,S} = 0.73$ $D_V = 16 \text{ mm}$

Experiment: Inova vs. MATS

Location: CTU, Czech Republic Capacity: 2.5 MN Special feature: rapid unloading



NTU, Taiwan 60 MN 6 independent DOFs



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Experiment: e = 100 mm, $\hat{e} = 0.5$



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Material models

• **Concrete:** Con2DPM *CDPM2:* A damage-plasticity approach to modelling the failure of concrete (Grassl et al. 2013)

$$\begin{split} \bar{\boldsymbol{\sigma}} &= \mathsf{D}_{\mathrm{e}} : \left(\varepsilon - \varepsilon_{\mathrm{p}}\right) \\ \boldsymbol{\sigma} &= \left(1 - \omega_{\mathrm{t}}\right) \bar{\boldsymbol{\sigma}}_{\mathrm{t}} + \left(1 - \omega_{\mathrm{c}}\right) \bar{\boldsymbol{\sigma}}_{\mathrm{c}} \end{split}$$



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• **Concrete:** Con2DPM *CDPM2:* A damage-plasticity approach to modelling the failure of concrete (Grassl et al. 2013)

• Reinforcement: MisesMat Mises plasticity + isotropic damage + linear isotropic hardening)

$$\sigma = (1 - \omega)\overline{\sigma} = (1 - \omega)\mathsf{D}(\varepsilon - \varepsilon_{\rm p})$$
$$f(\overline{\sigma}, \kappa) = \sqrt{3J_2(\overline{\sigma})} - \sigma_{\rm Y}(\kappa)$$
$$\sigma_{\rm Y}(\kappa) = \sigma_0 + H\kappa$$
$$\omega(\kappa) = \omega_c(1 - e^{-a\kappa})$$



Computational models

- Representative section
 - indirect displacement control
 - top surface: weighted master-slave condition
 - reinforcement: linear truss elements
 - concrete-reinforcement interaction: hanging nodes



Computational models

- Representative section
- Symmetric half
 - complex reinforcement geometry
 - direct displacement control
 - geometrically nonlinear using nlgeo 1
 - reinforcement Truss3dNL ...nlgeo 1



Computational models

- Representative section
- Symmetric half
- Engineering model
 - NonLinearStatic
 - elastic stiffness matrix, initial guess
 - DSS solver, OpenMP



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Results: representative section, CDPM2 vs. design codes



Results: MSR vs. longitudinal reinforcement





Results: MSR, axial compression



- 1 Unconfined concrete
- 2 Single-confined concrete, large spiral
- 3 Single-confined concrete, small spiral
- 4 Double-confined concrete
- 5 Reduced confinement

Results: mesh sensitivity



Results: mesh sensitivity



	[-]
v. coarse, $8 \times 8 \times 2$	21
coarse, $16 imes 16 imes 4$	168
medium, $32 \times 32 \times 8$	1 518
fine, $46 \times 46 \times 12$	5 284











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Results: axial strain and curvature, $\hat{e} = 0.5$ (e = 100 mm)



Results: axial strain and curvature, $\hat{e} = 1.0$ (e = 200 mm)



Experiment: layout of displacement sensors





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Results: ID, representative section vs. symmetric half vs. experiment



Results: FEM vs. experiment





Computational model







- In the case of longitudinal reinforcement only, the numerical results obtained with the representative section approach and CDPM2 material model comply with the design codes. The MSR reinforcement enhances strength from ≈ 25% (high eccentricity) to 40% (low eccentricity).
- The peak load is reached at the onset of spiral yielding, which corresponds to the maximum confinement.
- A considerable mesh dependence of the MSR simulations has been detected. The explanation was found in the behavior of the zone with *reduced confinement*, just outside the small spirals. Coarser meshes lead to strength overestimation because this effect is not considered properly.
- Second-order moments are important in both experiments and modeling. An exceptional agreement between the experiments and numerical results was obtained, which proves the superior performance of MSR layout stemming from laterally confined concrete.



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Future goals

- 2 outputs for CeSTaR 2 project
- 1 Formulae for the design of columns with MSR
 - Mechanical response of compressed concrete columns with two interlocking circular spirals (bachelor thesis of Marketa Venclova) + experiments





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- 2 outputs for CeSTaR 2 project
- $1\,$ Formulae for the design of columns with MSR
 - Mechanical response of compressed concrete columns with two interlocking circular spirals (bachelor thesis of Marketa Venclova) + experiments
- 2 MaLCoLM 2.0 (Multi-spiral column simulation module, OOFEM extension module)
 - PySide (LGPL) = Python Qt bindings
 - OOFEM python bindings (full or partial?)
 - primary purpose: quick design + interaction diagram

Thank you for your attention.

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